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## A New On-Land Seismogenic Structure Source Database by the Taiwan Earthquake Model (TEM) Project for Seismic Hazard Analysis of Taiwan

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27 **ABSTRACT**

28 Taiwan is located at an active plate boundary and is prone to earthquake hazards.  
29 To evaluate the seismic risk of the island, the Taiwan Earthquake Model (TEM)  
30 project, supported by the Ministry of Sciences and Technology, aims for obtaining  
31 earthquake hazard, risk, and related social and economic impact models of Taiwan  
32 through multidisciplinary collaborations. One of the major tasks of TEM is to  
33 construct a complete and updated seismogenic structure database for Taiwan to assess  
34 future seismic hazards. Toward this end, we have combined information from  
35 pre-existing databases and data obtained from new analyses to build an updated and  
36 digitized three-dimensional seismogenic structure map for Taiwan. 38 on-land  
37 active seismogenic structures are identified. Furthermore, for detailed information  
38 of individual structures such as their long-term slip rates and potential recurrence  
39 intervals, we have collected the data from existing publications, as well as calculated  
40 from results of our own field surveys and investigations. We hope this updated  
41 database would become a significant constraint for the calculations of seismic hazard  
42 assessments in Taiwan, and would provide important information for engineers and  
43 hazard mitigation agencies.

44

45 **Keywords:** Taiwan Earthquake Model (TEM), seismic hazard analysis, seismogenic  
46 structure, database, slip rates, recurrence intervals.

47

## 48 1. INTRODUCTION

49

50 The island of Taiwan is the result of the ongoing collision between the Eurasian and  
51 Philippine Sea plates (Fig. 1). Rapid rates of both horizontal and vertical  
52 deformation and an abundance of seismic activity amply demonstrate the current  
53 vigor of the orogeny. The 1999 Chi-Chi earthquake, with its unanticipated  
54 disastrous effects on population and infrastructure, focused much scientific and public  
55 attention on Taiwan and demonstrated the urgent need for a better understanding of  
56 the island's numerous other seismogenic structures and future earthquake hazards  
57 (e.g., Cheng et al., 2007, 2010). In order to obtain more information toward  
58 fulfilling this need, the integrated project of Taiwan Earthquake Model (TEM) has  
59 been carried out with a goal to put together information for seismic hazard assessment  
60 and risk management for the island. One of the most fundamental tasks of TEM is  
61 to construct an up-to-date database of seismogenic structures of Taiwan.

62 There have been several previous efforts to construct the active structure database of  
63 Taiwan (e.g., Shyu et al., 2005; Central Geological Survey, 2010). However, some  
64 of these databases include only active faults that produce observable offset at the  
65 surface, without structures that only produced tectonic geomorphic features but not  
66 yet ruptured the surface. Moreover, a seismogenic structure database for seismic  
67 hazard calculation needs many structural parameters. These parameters include  
68 physical characteristics of the structures such as their types and geometries, those  
69 obtained by geological investigations such as their slip rates, as well as calculated  
70 parameters related with the earthquakes they may produce, such as the earthquake  
71 magnitudes and average recurrence intervals. Since some of these parameters are  
72 difficult to obtain, a dataset with all parameters of the structures is still lacking.

73 Toward this end, we have reviewed pre-existing active structure databases and related  
74 reports in order to construct a more complete seismogenic structure database for  
75 Taiwan. For example, the Central Geological Survey (CGS) of Taiwan has  
76 investigated many active faults in Taiwan by a wide variety of methods, including  
77 outcrop mapping, trenches, seismic investigations, and the integration of historical  
78 documents. They have assembled these data to publish several versions of active  
79 fault maps of Taiwan (e.g., Chang et al., 1998; Lin et al., 2000; Central Geological  
80 Survey, 2010). These maps focus especially on faults that crop out at the surface,  
81 such as the Chelungpu fault that ruptured in 1999 and produced the Chi-Chi  
82 earthquake. The 1999 rupture, in fact, followed a pre-existing topographic scarp that  
83 can be identified even before the earthquake (e.g., Chen et al., 2002; Chang and Yang,  
84 2004). Such phenomenon inspired Shyu et al. (2005) to review all geomorphic  
85 features in detail, and to produce a neotectonic map of Taiwan with the additional aid  
86 from geodetic and seismologic data. This dataset not only includes faults that crop  
87 out at the surface, but also considers structures that are blind but expressed  
88 geomorphically.  
89 Several structural parameters are also reported in Shyu et al. (2005). For example,  
90 geometries of the structures are constrained either by seismic data or by the depth of  
91 an assumed brittle-ductile transition. These parameters can be further used to  
92 estimate the possible magnitude of earthquakes produced by these structures using  
93 empirical equations (e.g., Wells and Coppersmith, 1994). However, in order to  
94 calculate seismic hazard for TEM, more information is needed. The average  
95 recurrence interval of earthquake produced by the structure, for instance, is a key  
96 parameter for calculating seismic hazards. Such information may be obtained by  
97 paleoseismological investigations (e.g., Chen et al., 2007), but not all structures in  
98 Taiwan have been trenched. Alternatively, for structures with constrained long-term

99 slip rates, the recurrence interval can be calculated from the slip rates and the average  
100 slip amount, which can be estimated from the earthquake magnitude or from  
101 empirical equations (e.g., Wells and Coppersmith, 1994).  
102 Therefore, in this study, we have constructed a new seismogenic structure database by  
103 integrating and re-interpreting previous databases, and by combining previously  
104 published information for the structural parameters. For those without previous  
105 information, we provide our new estimations. Since the long-term slip rates for most  
106 of the structures are not well constrained previously, we have especially focused on  
107 the estimation of slip rates of structures from geomorphic and field investigations in  
108 this study. It is noteworthy that this result represents only an updated version of such  
109 dataset based on the most current knowledge. As pointed out by Shyu et al. (2005)  
110 in one of the earlier versions of such database, we by no means suggest that all  
111 seismogenic structures or related information are constrained and described in this  
112 dataset. Decades of additional work and regular updates would be necessary to  
113 accomplish such goals as new information becomes available. With these caveats in  
114 mind, we present in this study a first version of such database, and hope our results  
115 not only can provide important constraints for the seismic hazard calculations of TEM,  
116 but can also assist in future land-use and other planning programs in Taiwan.

117

## 118 2. FIELD INVESTIGATIONS

119

120 As long-term slip rates of many structures were not constrained previously, we have  
121 conducted intensive field investigations to obtain the structures' long-term slip rates.  
122 Such information can be applied further to calculate potential recurrence interval of  
123 earthquakes produced by each seismogenic structure. In fact, more than half of the  
124 structures included in this new database do not have any published slip rate or

125 recurrence interval information. As a result, we utilize the topographic features of  
126 these structures to estimate reasonable long-term slip rates for them.

127 Many of the structures included in the database have produced distinctive deformation  
128 of young geomorphic surfaces, such as fluvial or marine terraces. Indeed, scarps that  
129 cut across widespread fluvial terraces are one of the fundamental features for the  
130 identification of active structures in Taiwan (e.g., Shih et al., 1984, 1986; Yang, 1986;  
131 Shyu et al., 2005). Such structural scarps can be distinguished from erosional terrace  
132 risers since the latter would generally follow the flow direction of the rivers, whereas  
133 scarps produced by active deformation can trend at an angle with the rivers and are  
134 generally parallel to the mountain front (Fig. 2). Once we obtain the amount of total  
135 deformation and the age of the deformed surface, we will be able to calculate a  
136 long-term deformation rate of the structure.

137 The amount of deformation is generally determined by the height of the structural  
138 scarp. This is based on the hypothesis that the two surfaces on both sides of the  
139 scarp have the same age. Therefore, we need to pay additional attention to exclude  
140 the possibility of later erosion of the upthrown side or deposition on the downthrown  
141 side. In cases such possibility cannot be excluded, the amount of deformation  
142 determined will be just the minimum. For the height of the scarps, we measured  
143 them both in the field by a laser range finder and from the Digital Elevation Model  
144 (DEM) with 5-m resolution. Both results are compared with each other, and we  
145 found that generally the measurements from DEM are higher than those obtained in  
146 the field. This is likely due to the fact that our measured length in the field was not  
147 long enough to cover the entire deformation zone. **As a result, we used the data from  
148 DEM measurements for most of the structures, in order to obtain a more complete  
149 deformation amount of the structures.**

150 The ages of the deformed surfaces are, however, much more difficult to determine.

151 Ideally, one would like to date all of those deformed terrace sediments to obtain their  
152 ages. However, in reality datable materials are difficult to come across in the field.  
153 More importantly, many of the older terraces in Taiwan are older than the upper limit  
154 of radiocarbon dating method (e.g., Chen, 1988; Lee et al., 1999; Ota et al., 2002;  
155 Shyu et al., 2006a), which is the most reliable and well-developed dating method.  
156 It has been reported that in Taiwan, terraces with initial development of reddish, or  
157 lateritic, soil at their surface generally have ages about 30-40 ka, near the upper limit  
158 of radiocarbon dating method (e.g., Chen, 1988; Ota et al., 2002). The degree of  
159 lateritic development will increase as the terraces become older due to a longer period  
160 of weathering (e.g., Tsai et al., 2007). On the other hand, the best developed lateritic  
161 soil in Taiwan is present at the top surface of the Linkou Tableland (e.g., Lee et al.,  
162 1999; Fig. 1). This tableland is preserved on the upthrown side of a normal fault,  
163 and the oldest sediment on the downthrown side has been determined to be at least  
164 400 kyr old (Wei et al., 1998). Based on the information above, we decided to  
165 categorize all fluvial terrace surfaces in Taiwan in order to provide a reasonable  
166 estimation of their ages. For lateritic terraces there are two categories. Those with  
167 less developed lateritic soil are assigned an age of 30-150 ka, and those with  
168 well-developed lateritic soil are assigned an age of 100-500 ka. For non-lateritic  
169 terraces there are also two categories. For those very young terraces without any soil  
170 development, an age of 1-5 ka is assigned. If there is some soil development at the  
171 surface but the color of the soil has not yet turned red, we assign an age of 5-25 ka for  
172 such terraces (Fig. 3). We have intentionally set a large error bar for these  
173 estimations, at 5 times of the youngest ages. This is a conservative approach based  
174 on current understandings, and will of course be improved as more information  
175 becomes available. Moreover, this would be the first systematic estimation for all  
176 terrace ages in Taiwan. Without such estimation, it would be impossible to



177 reasonably calculate the seismic hazards of Taiwan, since sometimes unrealistic  
178 extreme values were also considered in some previous models.

179

### 180 **3. SEISMOGENIC STRUCTURES OF TAIWAN AND THEIR** 181 **PARAMETERS**

182

183 After determining the slip rates of all structures, we are able to construct a new  
184 on-land seismogenic structure database for Taiwan, with all important structural  
185 parameters (Fig. 4 and Table 1). A more detailed structural parameter table and the  
186 ArcGIS shapefiles of all the structures are included in the supplementary files of this  
187 paper.

188 For the geometries of the structures, one of the fundamental parameters is the  
189 down-dip limit of each structure. In this study, we started by following the approach  
190 of Shyu et al. (2005) to estimate the depth of the brittle-ductile transition. As  
191 pointed out by Shyu et al. (2005), most of the rocks in the upper crust of Taiwan are  
192 quartz- and feldspar-rich sedimentary rocks. Since the brittle-plastic transition of  
193 quartz occurs at approximately 300°C (e.g., Kerrich et al., 1977; Tullis and Yund,  
194 1977), and that of feldspar occurs at approximately 500°C (e.g., White, 1975; Tullis  
195 and Yund, 1977), Shyu et al. (2005) used a conservative depth of 15 km (~450°C) for  
196 the down-dip limit of most structures in Taiwan.

197 Some of the seismogenic structures in western Taiwan, however, do not seem to cut  
198 the crust to the depth of the brittle-ductile transition. Instead, many of them appear  
199 to stop at, or merge with a shallow detachment (e.g., Suppe, 1976, 1987; Carena et al.,  
200 2002). Therefore, for those structures that their seismogenic depths have been well  
201 illuminated either by published seismic investigation data or distribution patterns of  
202 seismicity, we used such better constrained information.

203 For other structures that may indeed extend to the brittle-ductile transition, we  
204 followed the temperature proposed by Shyu et al. (2005), but used new geothermal  
205 gradient data of Taiwan to calculate the actual depth of such temperature. Several  
206 new geothermal gradient datasets of Taiwan have become available in recent years,  
207 including one using the Curie point depth from magnetic data in Taiwan (Hsieh et al.,  
208 2014) and one using silica heat flow geothermometry from hot springs (Liu et al.,  
209 2015). The geothermal gradients proposed by Hsieh et al. (2014) appear to be higher,  
210 especially for the south and southeastern part of Taiwan. As a result, the depths of  
211 the brittle-ductile transition calculated using this dataset are shallower than 10 km for  
212 almost all structures in Taiwan. This appears to be inconsistent with the observation  
213 of numerous seismicity in Taiwan below the depths of 10 km (e.g., Wu et al., 1997;  
214 Rau and Wu, 1998). Therefore, we decided to calculate the depths of the  
215 brittle-ductile transition in Taiwan using the dataset proposed by Liu et al. (2015),  
216 which yielded results generally between 10 and 15 km (see the detailed structural  
217 parameter table in the supplementary files). Since the contours of geothermal  
218 gradient shown in Liu et al. (2015) have an interval of 3.75°C and most of the  
219 structures are located in areas with geothermal gradient between 30 and 45 °C/km, the  
220 seismogenic depth calculated in this study would have error bars in the range of ~1 to  
221 1.5 km.

222 After we obtained the seismogenic depth of each structure, we then construct the  
223 general geometries of the structures. These geometries were further checked for any  
224 possible conflicts using our 3-dimensional structural model described below.

225 The moment magnitudes ( $M_w$ ) of earthquakes likely produced by these structures  
226 were calculated using published regression results from Wells and Coppersmith  
227 (1994), and we can further use this information to obtain the average slip per  
228 earthquake event through the calculation of the seismic moment. Finally, the

229 average recurrence intervals of such earthquakes were calculated from the average  
230 slip per event and the slip rates of the structures.

231 In this new seismogenic structure database, 38 structures were identified. The  
232 following is the general information of each structure:

- 233 1. The Shanchiao fault is located near the Taipei City with a length of 53.4 km. It is  
234 a listric fault, with a dip of  $60^\circ$  between 0-7 km deep and  $45^\circ$  from 7 to 10 km  
235 deep. Then it dips at  $30^\circ$  to a depth of 13.8 km. The vertical deformation rate  
236 is 2.25 mm/yr from Huang et al. (2007), and we calculated a slip rate of  $1.85 \pm$   
237  $0.76$  mm/yr in this study based on the estimation of the age of the Linkou  
238 Tableland on its upthrown side.
- 239 2. The Shuanglienpo structure is near Taoyuan with a length of 9.0 km. Its dip is  
240  $45^\circ$  until 3 km deep then becomes  $15^\circ$  to a depth of 5 km. Its slip rate is  
241 estimated at  $0.25 \pm 0.17$  mm/yr in this study.
- 242 3. The Yangmei structure is southeast of the Shuanlienpo structure, and its length is  
243 21.7 km. It dips  $60^\circ$  and extends to a depth of 3 km. We estimated its slip rate  
244 at  $0.38 \pm 0.26$  mm/yr.
- 245 4. The Hukou fault is parallel to the Yangmei structure. This fault is 25.8 km in  
246 length, dips at  $30^\circ$ , and extends to 10 km deep. In previous studies, the slip rate  
247 was estimated at  $1.65 \pm 0.15$  mm/yr based on a 50 m scarp height and an age of  
248  $60.9 \pm 5.5$  ka of the deformed terrace (Shen et al., 2005; Chen et al., 2006). We  
249 estimated a slip rate of  $1.16 \pm 0.84$  mm/yr in this study.
- 250 5. The Fengshan river strike-slip structure is a structure that appears to cut the  
251 Hukou fault. The length of this structure is 30.4 km, and we propose a dip of  $80^\circ$   
252 for the structure, with a depth of 13.9 km. We estimated its slip rate at  $3.61 \pm$   
253  $2.41$  mm/yr.
- 254 6. The Hsinchu fault is located near the downtown of Hsinchu. The depth of the

255 fault is 10 km with a 45° dip, and its length is 12.6 km. A slip rate of 0.45 mm/yr  
256 is reported previously (Chen et al., 2004), and we estimated at  $0.70 \pm 0.46$  mm/yr  
257 in this study.

258 7. The Hsincheng fault is another important structure in the Hsinchu area. It is 13.0  
259 km in length, dips at 30°, and extends to 12.9 km. Previous reported slip rates of  
260 the fault include 0.7-1.6 mm/yr (Shih et al., 2003) or  $1.075 \pm 0.025$  mm/yr based  
261 on optically stimulated luminescence (OSL) ages of deformed terraces (W.-S.  
262 Chen et al., 2003). We estimated a slip rate of  $1.08 \pm 0.72$  mm/yr for the fault.

263 8. The Hsinchu frontal structure is near the coastline of the Hsinchu area. Its length  
264 is 10.4 km, dip is 30°, and it extends to 10.0 km deep. In this study, we obtained  
265 a slip rate of  $2.80 \pm 1.86$  mm/yr.

266 9. The Touhuanping structure is in the Miaoli area, and its length is 24.8 km. It  
267 dips at 85° and extends to a depth of 12.0 km. We calculated a slip rate of 0.13  
268 mm/yr based on a published age constraint of the deformed terraces (Ota et al.,  
269 2009).

270 10. The Miaoli frontal structure is near the coastline of the Miaoli area. Its length is  
271 20.8 km, dip is 30°, and it extends to a depth of 10.0 km. In this study, we  
272 obtained a slip rate of  $3.60 \pm 2.40$  mm/yr.

273 11. The Tunglo structure is a north-south striking structure in the Miaoli area. The  
274 depth of the down-dip limit of this structure is 3.5 km, with the dip of the structure  
275 at 30° and the length at 11.1 km. The slip rate is estimated at  $1.08 \pm 0.72$  mm/yr  
276 in this study.

277 12. The East Miaoli structure is another north-south striking structure in the Miaoli  
278 area. It dips at 30° with a length of 14.1 km. We calculated a slip rate of  $1.60 \pm$   
279  $1.06$  mm/yr for this structure.

280 13. The Shihtan fault is the seismogenic fault of the M7.1 Hsinchu-Taichung

281 earthquake in 1935 (Hayasaka, 1935; Otuka, 1936). The length of the fault is  
282 28.6 km. The fault dips at 75° to a depth of 10.8 km. According to our  
283 estimation, the slip rate of the fault is  $1.86 \pm 1.24$  mm/yr.

284 14. The Sanyi fault is also in the Miaoli area. The geometry of this fault include a  
285 length of 27.2 km, a dip of 15°, and a down-dip limit at 9.0 km deep. In this  
286 study, the slip rate is estimated at  $1.86 \pm 1.23$  mm/yr.

287 15. The Tuntzuchiaio fault is also related with the Hsinchu-Taichung earthquake in  
288 1935 (Otuka, 1936). It has a length of 25.1 km. We speculated an 85° dipping  
289 of the fault that extend to a depth of 14.8 km. From these data, we estimated its  
290 slip rate at  $1.00 \pm 0.68$  mm/yr.

291 16. The Changhua fault is located along the front of a series of tablelands in central  
292 Taiwan. It is also a listric fault, with a dip of 45° from 0 to 3 km deep, 30° from  
293 3 to 5 km deep, and finally 10° from 5 to 12.00 km deep. Previous estimated slip  
294 rates of this fault include  $6.18 \pm 0.10$  mm/yr constrained by uplifted terraces (Ota  
295 et al., 2002) and 1.7-10.3 mm/yr from borehole data (Chen et al., 2008a). In this  
296 study, its slip rate is estimated at  $3.40 \pm 2.26$  mm/yr.

297 17. The Chelungpu fault is one of the best known faults in Taiwan, since it is the  
298 seismogenic fault of the 1999 Chi-Chi earthquake. We have used information  
299 obtained from many previous studies of the fault in this database.

300 18. The Tamaopu-Shuangtung fault is sub-parallel to the Chelungpu fault and to its  
301 east. The length of the fault is 68.7 km. It dips at 30° and extends to a depth of  
302 6.0 km. We estimated its slip rate at  $2.00 \pm 1.34$  mm/yr.

303 19. The Chiuchiungkeng fault is at the boundary between the hills and the coastal  
304 plain in the Chiayi area. The slip rates were reported between 0.28 and 13.7  
305 mm/yr in previous studies (Chen et al., 2006; Lin et al., 2007). Its length is 32.9  
306 km and it dips at 30° to a depth of 12.0 km. The slip rate is estimated at  $7.20 \pm$

307 4.80 mm/yr in this study.

308 20. The length of the Meishan fault is 24.0 km. Rupture of this fault produced a  
309 M7.1 earthquake in 1906 (Omori, 1907). Its dip is  $85^\circ$  to a depth of 14.7 km.  
310 We estimated a slip rate of 2.51 mm/yr in this study.

311 21. The Chiayi frontal structure is a blind fault beneath the coastal plain of the Chiayi  
312 and Tainan areas. The length of this structure is 44.3 km, with a dipping angle of  
313  $15^\circ$  to a depth of 12.0 km. The slip rate of this structure is estimated at  $6.49 \pm$   
314  $4.33$  mm/yr.

315 22. The Muchiliao-Liuchia fault is also at the front of the hills in the Chiayi and  
316 Tainan areas. The length of the fault is 24.9 km, and the dip is  $30^\circ$ . Previous  
317 reported slip rate of the fault is between 4.7 and 12.78 mm/yr (Yang et al., 2005;  
318 Chen, 2006; Du, 2013). We calculated its slip rate at  $5.75 \pm 1.35$  mm/yr.

319 23. The Chungchou structure is east of the Tainan City. Its length is 29.7 km, its dip  
320 is  $30^\circ$ , and the structure extends to a depth of 12.0 km. Chen and Liu (2000) and  
321 Chen (2010) used borehole data to calculate the uplift rate of the upthrown side of  
322 this structure, and their results are between 5 and 8 mm/yr. In this study, we  
323 have thus calculated its slip rate at  $12.20 \pm 0.60$  mm/yr.

324 24. The Hsinhua fault is near the Chungchou structure, and rupture of this fault  
325 produced the M6.3 earthquake in 1946 (Chang et al., 1947; Bonilla, 1977). Its  
326 length is 14.1 km, and it dips at  $85^\circ$  to a depth of 15 km. The uplift rate of the  
327 upthrown side has been reported at 0.8-4.5 mm/yr (Chen et al., 2011), and we  
328 estimated a slip rate of  $2.65 \pm 1.85$  mm/yr for this fault in this study.

329 25. The Houchiali fault is in the Tainan City proper with a length of 11.5 km. It dips  
330 at  $45^\circ$  and extends to 5.0 km deep. Based on borehole data, Chen and Liu (2000)  
331 obtained an uplift rate of its upthrown side at 6 mm/yr. Thus we estimated a slip  
332 rate of 8.49 mm/yr for this fault in this study.

333 26. The Chishan fault is southeast of Tainan. This fault is 34.8 km in length, dips at  
334 75°, and extends to a depth of 10.8 km. Whereas Chen et al. (2012) estimated a  
335 slip rate of  $0.75 \pm 0.25$  mm/yr for this fault, in this study we calculated its slip rate  
336 at  $1.10 \pm 0.36$  mm/yr.

337 27. The Hisaokangshan fault is west of the Chishan fault. It is likely dipping at 30°  
338 to a depth of 7.0 km. Chen et al. (2008b) reported that the fault has a slip rate of  
339  $6.2 \pm 0.8$  mm/yr. In this study, its slip rate is estimated at  $3.30 \pm 2.20$  mm/yr.

340 28. The Kaoping River structure is identified by a linear scarp at the western side of  
341 the Kaoping River. Its length is 29.2 km, and it dips at 75° to a depth of 12.3  
342 km. The slip rate that we calculated is  $0.61 \pm 0.41$  mm/yr.

343 29. The Chaochou fault at the eastern side of the Pingtung Plain forms the boundary  
344 between the southern Central Range and the plain. The length of this fault is  
345 79.6 km. It dips at 75° and extends to a depth of 11.1 km. The slip rate of the  
346 fault is estimated at  $1.76 \pm 1.17$  in this study.

347 30. The Hengchun fault is one of the southernmost structures in Taiwan. The length  
348 of this fault is 37.2 km, and the fault dips at 75° and extends to a depth of 15.0 km.  
349 Based on the dating result of marine terraces, Chen et al. (2010) calculated an  
350 uplift rate of  $4.2 \pm 0.2$  mm/yr for the upthrown side of the fault. Thus we  
351 estimated its slip rate at  $6.15 \pm 0.29$  mm/yr.

352 31. The Hengchun offshore structure is to the west of the Hengchun fault. It dips at  
353 30° and extends to a depth of 4.0 km. The length of this structure is 14.5 km,  
354 and the slip rate is estimated at  $3.65 \pm 1.11$  mm/yr in this study.

355 32. The Milun fault in eastern Taiwan is near the Hualien City. Rupture of this  
356 fault produced the M7.3 earthquake in October 1951 (Yang, 1953; Hsu, 1962).  
357 This fault has a length of 21.3 km, and it dips at 75° to 10.0 km deep. Chen  
358 (2013) calculated an uplift rate of  $6.93 \pm 0.03$  mm/yr of its upthrown side based

359 on U-Th dating results of corals found in uplifted marine terraces. Thus we  
360 estimated a slip rate of  $10.15 \pm 0.04$  mm/yr for the fault in this study.

361 33. The Longitudinal Valley fault is an important structure in eastern Taiwan, and  
362 forms the eastern boundary of the Longitudinal Valley. This fault is related with  
363 several historical earthquakes in eastern Taiwan, including the M7.0 earthquake  
364 series in November 1951 (Hsu, 1962; Cheng et al., 1996; Shyu et al., 2007).  
365 Seismicity of this fault also illuminated that it has a listric shape, dipping at  $75^\circ$  to  
366 a depth of 5.0 km,  $60^\circ$  between 5.0 and 15.0 km deep, and finally  $45^\circ$  to a depth of  
367 20.0 km. Several previous studies reported that the slip rate of the fault is  
368 between 20.5 and 32 mm/yr (Shyu et al., 2006b, 2008; Chen, 2006, 2010).  
369 However, this fault is also known for its aseismic creeping (e.g., Angelier et al.,  
370 1997; Lee et al., 2001). After considering its creeping rate, we estimated a slip  
371 rate of  $11.35 \pm 5.75$  mm/yr for the fault in this study.

372 34. The Central Range structure is located at the western edge of the Longitudinal  
373 Valley. It is 85.5 km long, dips at  $45^\circ$  to a depth of 20 km. We estimated a slip  
374 rate of  $7.28 \pm 1.77$  mm/yr in this study, based on published uplift rate estimations  
375 of its upthrown side (Shyu et al., 2006a).

376 35. The Luyeh Fault is located near the southern end of the Longitudinal Valley.  
377 With a length of 17.5 km, the fault dips at  $45^\circ$  to a depth of 2.0 km, then dips at  
378  $30^\circ$  to a depth of 4.0 km. Based on the ages of deformed terraces, it has been  
379 reported that the upthrown side of the fault has an uplift rate of 4.5 mm/yr (Shyu  
380 et al., 2008), and the fault has a slip rate of 5.4 mm/yr (Chen, 2010). We  
381 estimated a slip rate of  $6.34 \pm 0.17$  mm/yr for the fault in this study.

382 36. The Taimali coastline structure is along the coastline in southeastern Taiwan. Its  
383 length is 42.6 km, and the structure dips at  $75^\circ$  to a depth of 10.6 km. The slip  
384 rate of this structure is estimated at  $7.32 \pm 1.46$  mm/yr in this study.



385 37. We propose two structures bounding both side of the Ilan Plain in northeastern  
386 Taiwan. The one in the north is the Northern Ilan structure, with a length of 60.5  
387 km. It dips at 60° to a depth of 9.4 km. Based on borehole data, Su (2011)  
388 reported the vertical separation rate of this structure is 0.90-4.80 mm/yr. We  
389 used this information to obtain a slip rate of  $3.29 \pm 2.25$  mm/yr for this structure in  
390 this study.

391 38. South of the Ilan Plain is the Southern Ilan structure, with a length of 20.6 km. It  
392 dips at 60° to a depth of 11.3 km. We estimated its slip rate at  $5.48 \pm 0.64$  mm/yr  
393 based on the borehole data reported in Su (2011).

394

#### 395 4. 3-DIMENSIONAL SUBSURFACE MODEL OF THE STRUCTURES

396

397 In order to check for geometrical conflicts and to visualize the subsurface geometry of  
398 the seismogenic structures, we also constructed a three-dimensional subsurface model  
399 for these structures (Fig. 5). Furthermore, for structures that lack good depth  
400 constraints, the 3-D model also enabled us to estimate their proper down-dip limit.  
401 For example, some structures are proposed to originate from a single décollement,  
402 either as branches or as a thrust-backthrust system. The 3-D model would help us  
403 verify if such systems indeed merge at depth. For structures that are listric and have  
404 dipping angles changing at depth, the 3-D model is also helpful for visualizing such  
405 changes, as shown by the Changhua fault in Fig. 6. Similar characteristic is also  
406 found in the Shanchiao fault and the Longitudinal Valley fault.

407 This 3-D structural model is useful for the calculation of seismic hazards, since the  
408 distance-to-fault-plane data would be better constrained using such a model. The  
409 detailed datasets of this 3-D seismogenic structural model of Taiwan is included as a  
410 supplementary file of this paper.

411

## 412 5. DISCUSSION

413

414 As the first attempt to construct a complete seismogenic structure database by the  
415 TEM project, we have combined most of previously published structural parameters  
416 in the database. However, many of the parameters, especially the slip rates of the  
417 structures, have not yet been well constrained. As a result, we have also estimated  
418 the slip rates of structures based on our field investigations. Since many of the ages  
419 of deformed surfaces are unknown, we used a conservative approach to estimate those  
420 ages. This can be improved significantly as new information becomes available.  
421 For example, other dating methods such as OSL and cosmogenic nuclides (e.g., Y.-G.  
422 Chen et al., 2003; Siame et al., 2012) can be applied to determine the ages of older  
423 terraces. Such new data will lower the error bar of the age estimates, and will  
424 improve the precision of structural slip rates and average earthquake recurrence  
425 intervals.

426 Another issue of the structural slip rates is related to strike-slip structures. Most of  
427 the long-term slip rates were determined by vertical offset observed either in borehole  
428 data (e.g., Chen et al., 2008a) or by the deformation of surfaces (e.g., Shyu et al.,  
429 2008). However, the horizontal offsets by strike-slip structures are difficult to  
430 observe. A strike-slip offset of terrace risers helped us constrain the long-term slip  
431 rate of the Touhuanping structure (Ota et al., 2009), but many other pure strike-slip  
432 structures, such as the Meishan fault and the Hsinhua fault (Chen et al., 2011, 2013),  
433 lack such piercing points. More detailed investigations are needed to solve this issue  
434 in the future.

435 This seismogenic structure database is constructed on the basis of the structures'  
436 geomorphic manifestations. Therefore, for structures that do not have any

437 topographic features, we were unable to identify and include them in this database.  
438 During the past several years, however, several moderate earthquakes occurred on  
439 previously unidentified blind faults. A well-known example is the Mw 6.3 Jiasian  
440 earthquake that occurred on 4 March 2010, whose seismogenic structure appears to  
441 extend below 10 km deep and does not extend to the surface (Huang et al., 2011). A  
442 challenge for future versions of seismogenic structure databases would be how to  
443 identify and consider such blind structures.

444 In this study, we have mostly followed the results of Shyu et al. (2005) in the  
445 identification of active seismogenic structures. Although several other studies have  
446 proposed a few additional structures as active seismogenic structures, most of these  
447 structures do not show obvious geomorphic features. However, this may also  
448 indicate that these structures are slipping at lower rates than the rates of erosion or  
449 sedimentation, thus the deformation features have been obliterated or covered. Any  
450 ongoing or future efforts to update the seismogenic structure databases would need to  
451 focus on such structures, in order to further understand their current activities.

452 With all these caveats in mind, we have constructed the first version of a complete  
453 seismogenic structure database for Taiwan, with all structural parameters. This  
454 information has already been utilized as the seismogenic source model to calculate a  
455 first version of probabilistic seismic hazard analysis of Taiwan (Wang et al., submitted  
456 to this issue). As more data become available either through the ongoing TEM and  
457 other scientific research projects or as regular updating efforts by the government  
458 agencies, we hope the database will continue to improve, and provide better  
459 constraints for future seismic hazard assessments for Taiwan.

460

## 461 6. CONCLUSIONS

462

463 As part of the team effort of the Taiwan Earthquake Model project, we have combined  
464 previously published information and our field investigation results to construct a first  
465 complete on-land seismogenic structure database of Taiwan, with all structural  
466 parameters. 38 structures were identified in this study. We have also constructed a  
467 3-D subsurface structural model for the visualization of these structures. Such  
468 information will be useful for the calculation of seismic hazards of Taiwan. As more  
469 data become available, we hope the database will continue to improve and provide  
470 better constraints for future seismic hazard assessments for Taiwan.  
471

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689

690 **FIGURE CAPTIONS**

691

692 **Figure 1.** Major tectonic elements of the island of Taiwan. A, Western Foothills;  
693 B, Hsueshan Range; C, Central Range and Hengchun Peninsula; D, Longitudinal  
694 Valley; E, Coastal Range; F, western Taiwan coastal plains; G, Pingtung Plain; H, Ilan  
695 Plain; LkT, Linkou Tableland; KpR, Kaoping River.

696

697 **Figure 2.** The formation of a fault scarp. (a) If a fault has not moved for an  
698 extended period of time, erosional and sedimentary processes may have eliminate all  
699 previous topographic features of the fault. (b) However, if a fault moved recently, a  
700 fault scarp will be present next to the uplifted flood plain.

701

702 **Figure 3.** Our classification of soils on the terraces. (a) The degree of lateritic  
703 development will increase as the terraces become older due to a longer period of  
704 weathering. (b) An outcrop of a typical 1-5 kyr old terrace. (c) An outcrop of a  
705 typical 5-25 kyr old terrace. (d) An outcrop of a typical 30-150 kyr old terrace. (e)  
706 An outcrop of a typical 100-500 kyr old terrace. See text for more discussion.

707

708 **Figure 4.** Map of major seismogenic structures of Taiwan. The blue lines show  
709 the 38 structures in Taiwan.

710

711 **Figure 5.** Figures showing three-dimensional structural geometries below the  
712 surface. The geometries of the 38 structures are shown as colored polygons in the  
713 3-D model, and the background is the topography of Taiwan. The structural  
714 geometries are constrained mostly by seismic data from the Chinese Petroleum

715 Corporation (CPC), Taiwan, as well as the geothermal gradient data from Liu et al.  
716 (2015). Numbers correspond to the structure number in Fig. 4 and Table 1, and  
717 colors of the patches represent structures in different areas of Taiwan.

718

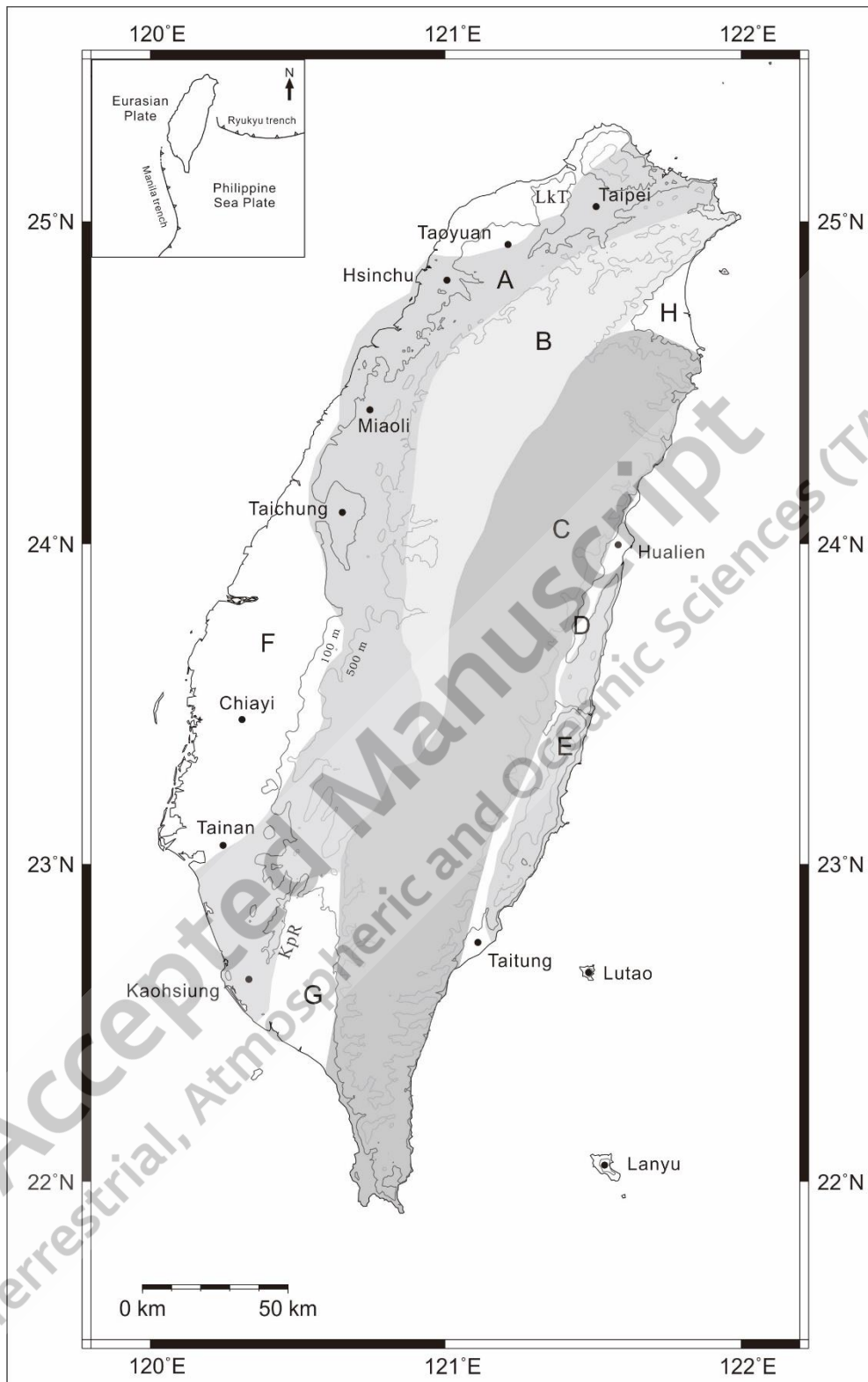
719 **Figure 6.** The geometry of the listric Changhua fault. The Changhua fault is listric  
720 based on previous studies, thus it is constructed using 3 segments of surfaces  
721 (between 0-3 km deep, 3-5 km deep, and 5-12 km deep) to show the varied dipping  
722 angle at different depths. Such approach is also applied to several other structures,  
723 such as the Shanchiao fault.

724

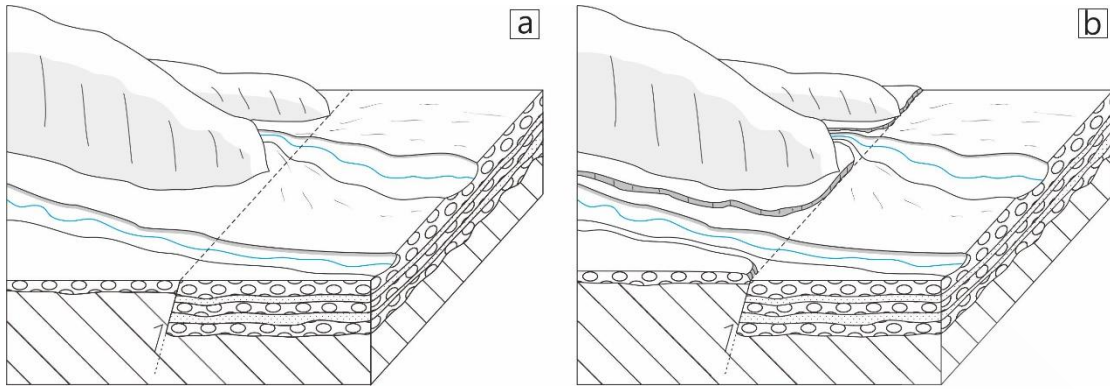
725 **Table 1.** The structural parameters of all seismogenic structures.

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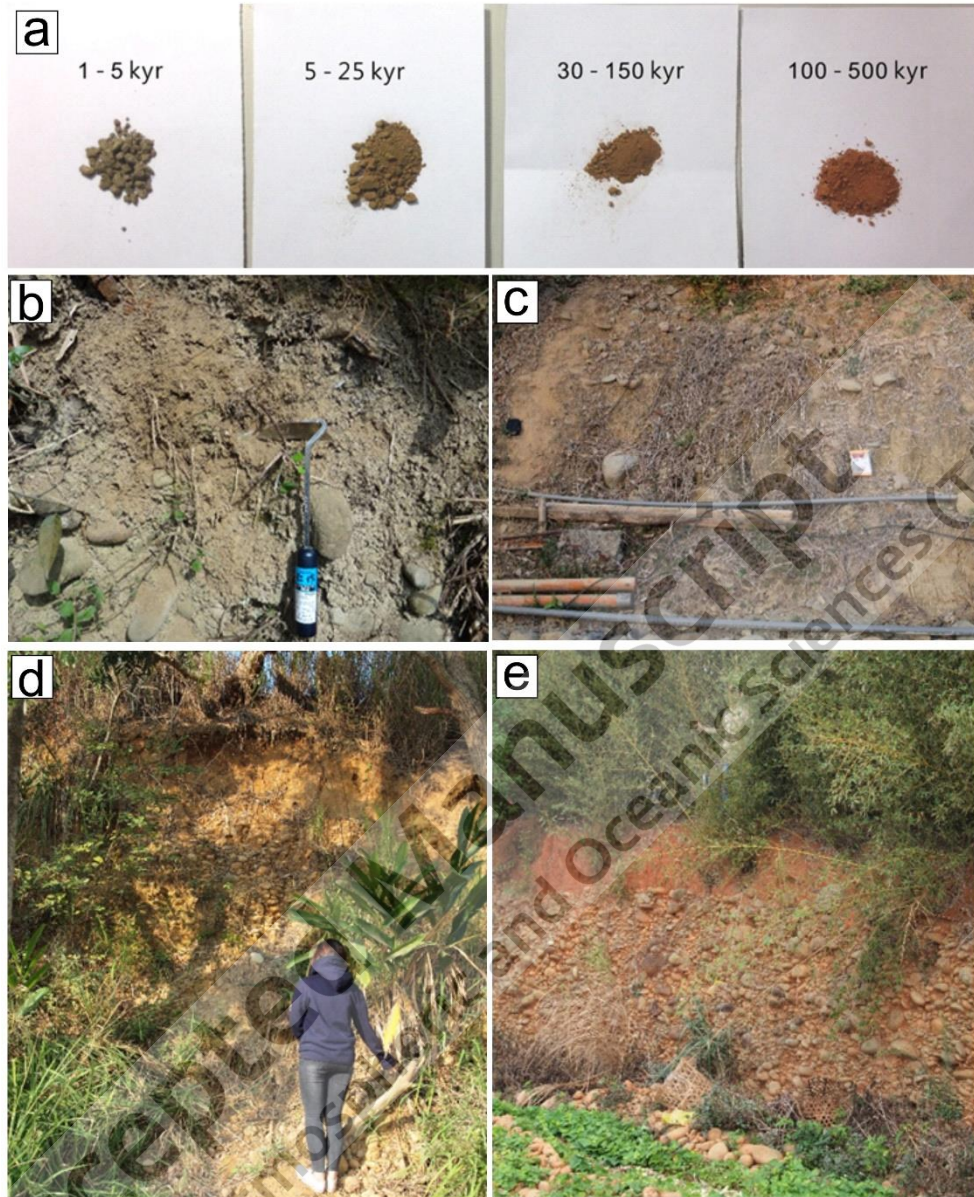
**Figure 1.** Major tectonic elements of the island of Taiwan. A, Western Foothills; B, Hsueshan Range; C, Central Range and Hengchun Peninsula; D, Longitudinal Valley; E, Coastal Range; F, western Taiwan coastal plains; G, Pingtung Plain; H, Ilan Plain; LkT, Linkou Tableland; KpR, Kaoping River.



**Figure 2.** The formation of a fault scarp. (a) If a fault has not moved for an extended period of time, erosional and sedimentary processes may have eliminated all previous topographic features of the fault. (b) However, if a fault moved recently, a fault scarp will be present next to the uplifted flood plain.

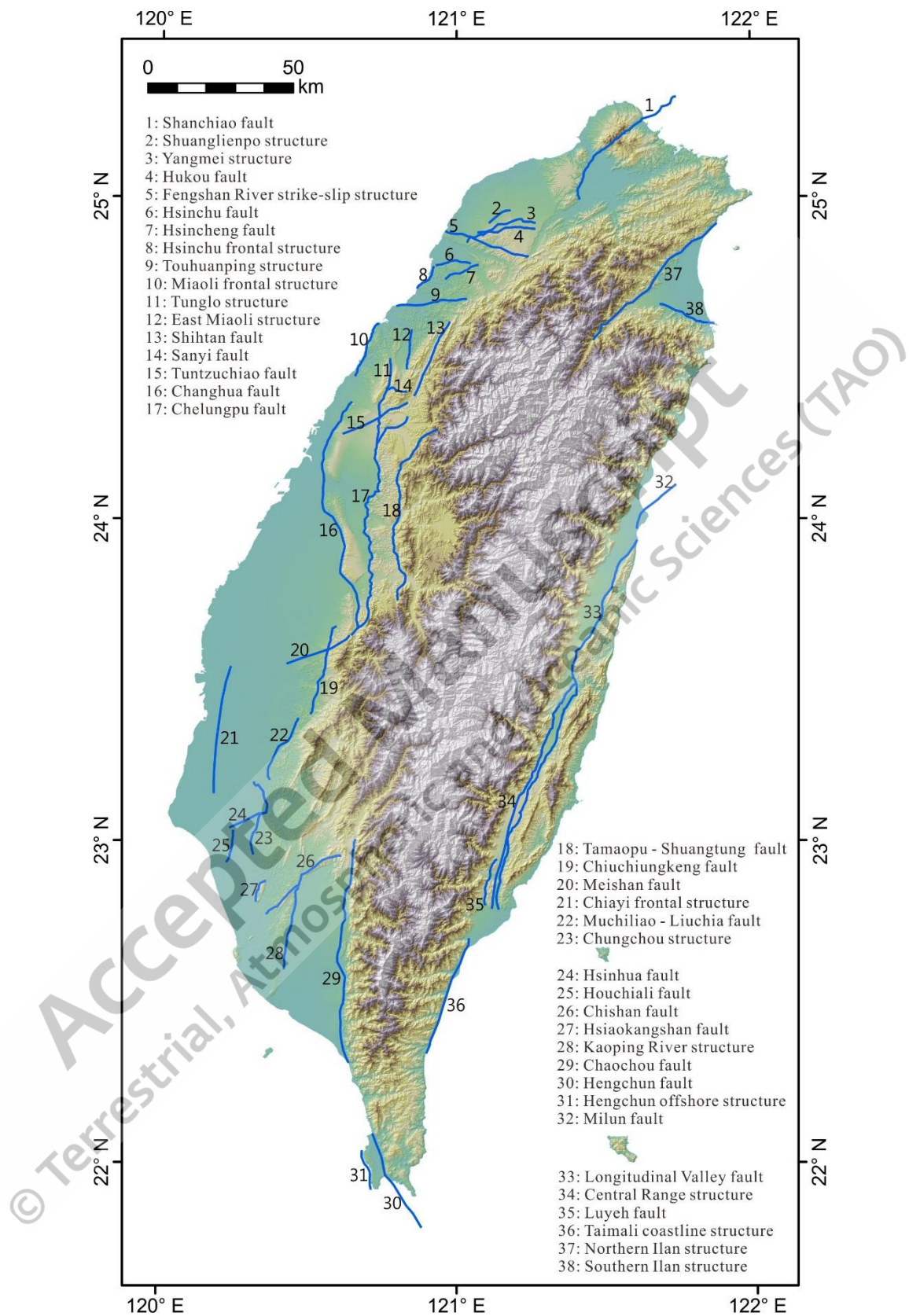
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**Figure 3.** Our classification of soils on the terraces. (a) The degree of lateritic development will increase as the terraces become older due to a longer period of weathering. (b) An outcrop of a typical 1-5 kyr old terrace. (c) An outcrop of a typical 5-25 kyr old terrace. (d) An outcrop of a typical 30-150 kyr old terrace. (e) An outcrop of a typical 100-500 kyr old terrace. See text for more discussion.





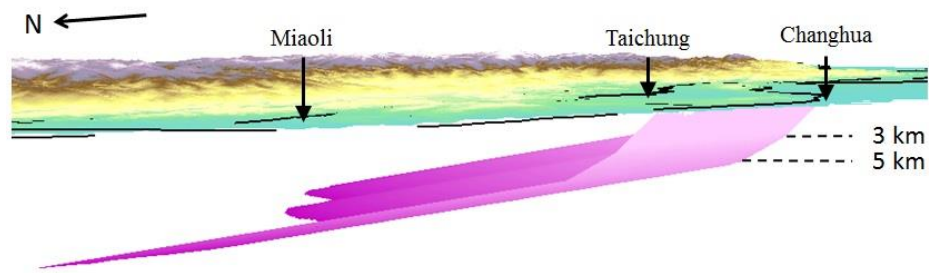
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**Figure 5.** Figures showing three-dimensional structural geometries below the surface. The geometries of the 38 structures are shown as colored polygons in the 3-D model, and the background is the topography of Taiwan. The structural geometries are constrained mostly by seismic data from the Chinese Petroleum

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**Figure 6.** The geometry of the listric Changhua fault. The Changhua fault is listric based on previous studies, thus it is constructed using 3 segments of surfaces (between 0-3 km deep, 3-5 km deep, and 5-12 km deep) to show the varied dipping angle at different depths. Such approach is also applied to several other structures, such as the Shanchiao fault.

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**Table 1.** The structural parameters of all seismogenic structures.

No.	Fault Name	Type <sup>#a</sup>	Length (km)	Width <sup>#b</sup> (km)	Area <sup>#c</sup> (km <sup>2</sup> )	M <sub>w</sub> <sup>#d</sup>	Displacement <sup>#e</sup> (m)	Slip rate <sup>#f</sup> (mm/yr)	Recurrence Interval <sup>#g</sup> (yr)
1	Shanchiao fault	N	53.40	19.84	1059.46	7.02	1.33	1.85 ± 0.76	510 – 1220
2	Shuanglienpo structure	R	9.00	11.97	107.73	6.16	0.67	0.25 ± 0.17	1600 – 8380
3	Yangmei structure	R	21.70	3.46	75.08	6.02	0.59	0.38 ± 0.26	920 – 4540
4	Hukou fault	R	25.80	20.00	516.00	6.77	1.15	1.16 ± 0.84	580 – 3600
5	Fengshan River strike-slip structure	SS	30.40	13.90	422.56	6.66	0.96	3.61 ± 2.41	160 – 800
6	Hsinchu fault	R	12.60	14.14	178.16	6.36	0.81	0.70 ± 0.46	690 – 3380
7	Hsincheng fault	R	13.00	25.71	334.23	6.60	0.99	1.80 ± 1.20	330 – 1650
8	Hsinchu frontal structure	R	10.40	20.00	208.00	6.42	0.85	2.80 ± 1.86	180 – 900
9	Touhuanping structure	SS	24.80	12.05	298.84	6.50	0.78	0.14	5570
10	Miaoli frontal structure	R	20.80	20.00	416.00	6.69	1.08	3.60 ± 2.40	180 – 900
11	Tunglo structure	R	11.10	7.00	77.70	6.03	0.59	1.08 ± 0.72	330 – 1640
12	East Miaoli structure	R	14.10	8.00	112.80	6.18	0.69	1.60 ± 1.06	260 – 1280
13	Shihtan fault	R	28.60	11.18	319.75	6.58	0.96	1.86 ± 1.24	310 – 1550
14	Sanyi fault	R	27.20	34.77	945.74	7.01	1.44	1.86 ± 1.23	470 – 2320
15	Tuntzuchiaofault	SS	25.10	14.85	372.74	6.60	0.88	1.00 ± 0.68	520 – 2670
16	Changhua fault	R	86.10	48.55	4180.15	7.59	2.41	3.40 ± 2.26	430 – 2130
17	Chelungpu fault	R	92.00	46.36	4265.12	7.60	2.44	6.94	350
18	Tamaopu - Shuangtung fault	R	68.70	12.00	824.40	6.95	1.34	2.00 ± 1.34	400 – 2030

19	Chiuchungkeng fault	R	32.90	24.00	789.60	6.94	1.35	7.20 ± 4.80	110 – 560
20	Meishan fault	SS	24.00	14.75	354.00	6.58	0.87	2.51	350
21	Chiayi frontal structure	R	44.30	46.36	2053.75	7.31	1.86	6.49 ± 4.33	170 – 860
22	Muchiliao - Liuchia fault	R	24.90	24.00	597.60	6.83	1.22	5.75 ± 1.35	170 – 280
23	Chungchou structure	R	29.70	24.00	712.80	6.90	1.30	12.20 ± 0.60	100 – 110
24	Hsinhua fault	SS	14.10	15.06	212.35	6.35	0.65	2.65 ± 1.85	140 – 810
25	Houchiali fault	R	11.50	7.07	81.31	6.05	0.61	7.07	86
26	Chishan fault	SS/R	34.80	11.18	389.06	6.62	0.91	1.10 ± 0.36	620 – 1250
27	Hsiaokangshan fault	R	9.00	14.00	126.00	6.22	0.70	3.30 ± 2.20	130 – 640
28	Kaoping River structure	SS/R	29.20	12.71	371.13	6.60	0.89	0.61 ± 0.41	870 – 4450
29	Chaochou fault	SS/R	79.60	11.50	915.40	7.00	1.43	1.76 ± 1.17	490 – 2420
30	Hengchun fault	SS/R	37.20	15.53	577.72	6.80	1.14	6.15 ± 0.29	180 – 200
31	Hengchun offshore structure	R	14.50	8.00	116.00	6.19	0.69	3.65 ± 1.11	140 – 270
32	Milun fault	SS/R	21.30	10.35	220.46	6.37	0.68	10.15 ± 0.04	70
33	Longitudinal Valley fault	R/SS	143.10	23.79	3404.35	7.51	2.24	11.35 ± 5.75	130 – 400
34	Central Range structure	R	85.50	28.28	2417.94	7.38	2.02	7.28 ± 1.77	220 – 370
35	Luyeh fault	R	17.50	6.83	119.52	6.20	0.69	6.34 ± 0.17	110
36	Taimali coastline structure	R/SS	42.60	10.93	465.62	6.73	1.11	7.32 ± 1.46	130 – 190
37	Northern Ilan structure	N	60.50	10.87	657.64	6.80	1.00	3.29 ± 2.25	180 – 960
38	Southern Ilan structure	N	20.60	12.99	267.59	6.41	0.64	5.48 ± 0.64	100 – 130



#a: R: reverse fault; SS: strike-slip fault; N: normal fault; SS/R: strike-slip dominated fault with minor reverse motion; R/SS: reverse dominated fault with minor strike-slip motion.

#b: Width equals to down-dip limit divided by the sine value of fault dip.

#c: Area of fault rupture equals to the Length times the Width.

#d: The moment magnitudes were calculated using the following equations: for reverse faults and reverse dominated faults,  $M_w = 4.33 + 0.90 * \log \text{Area}$ ; for strike-slip faults and strike-slip dominated fault,  $M_w = 3.98 + 1.02 * \log A$ ; for normal faults,  $M_w = 3.93 + 1.02 * \log A$  (Wells and Coppersmith, 1994).

#e: The average displacement (D) per event was calculated using the equation  $M_o = \mu AD$ , where  $\mu$  equals  $3*10^{11}$  dyne/cm<sup>2</sup>, A is the rupture area in #c,  $M_o$  was calculated from  $M_w$  by equation:  $M_w = 2/3 \text{ Log } M_o - 10.73$ .

#f: Slip rate is obtained from field investigations or previous studies. We measured the age and the vertical deformation amount of terraces to calculate the vertical deformation rate, and then calculated the slip rate (along the dip direction) by dividing the vertical deformation rate by the sine value of fault dip. For structures with multiple dip angles such as Shanchiao, Shuanglienpo, Changhua, Longitudinal Valley and Luyeh, the slip rates were calculated using the dip angle closest to the surface. For SS/R and R/SS structures, we assumed a 45° rake, thus the net slip rate would be  $\sqrt{2}$  times of the rate along the dip direction. For the Longitudinal Valley fault, we assume that the aseismic creeping rate is up to 3/4 of its total slip rate, thus we only used 1/4 - 3/4 of its total slip rate in the calculation.

#g: Recurrence interval equals Displacement divided by Slip rate.